glass WORLDWIDE Effect of coatings on adhesion of labels to glass containers

Adequate levels of hot end and cold end coatings are necessary to assure that non-refillable glass containers will move properly through high speed filling lines and to assure that the surface of these containers are adequately protected from becoming damaged during sliding contact. The current use of thin layers of tin oxide, applied immediately after forming while the glass is still hot and polyethylene, applied after the annealing process, is fully capable of achieving these objectives. However, if these coatings are improperly applied, performance problems of the coated containers can be observed. One such problem is the lack of adhesion of paper labels when using common glues. Gary Smay summarises the results of studies to determine the effect of tin oxide and polyethylene coatings on label adhesion when using casein-type glue.



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Non-refillable (NR) glass containers have been successfully used for over 50 years in the beverage, food, wine and spirit industries. These containers have less weight and corresponding thinner glass compared to their refillable counterparts, which requires that the outside surfaces of these containers are protected with hot end and cold end coatings. These coatings create both lubricious surfaces that enable the containers to move smoothly through filling lines and scratch resistance that maintains glass strengths at relatively high values(1).

When applied appropriately, these coatings do not cause any problems for either the manufacturer or the filler of glass containers. However, on rare occasions, some problems can arise. One of these potential problems concerns the adhesion of

labels to the glass surface. This study explores the effect that both hot end and cold end coatings have on proper label adhesion when using a casein-type adhesive that is typical of those used in the industry.

BACKGROUND

The methodology of depositing both hot end and cold end coatings onto the surface of NR glass containers has been well documented⁽²⁾. Currently, mono-butyl tin tri-chloride (MBTC) is the most common precursor material that is used to deposit tin oxide hot end coatings. When examined under high magnifications in an Atomic Force Microscope (AFM), this coating consists of individual globules of tin oxide that are randomly distributed across the glass surface, as shown in figure 1 (3). As measured thicknesses increase, both the size and number of these globules increase until a value of about 40 CTU is achieved, which coincides with complete coverage of the glass surface.

Once complete coverage is achieved, additional hot end coating simply adds to the depth of the physical thickness. In conjunction with the nature of the tin oxide coating, it has been observed that both the physical and chemical properties of the coating also change up to about 40 CTU, after which these characteristics remain constant with further increases in coating thicknesses (1,4,5). A slightly oxidised, low density form of polyethylene is the most common type of cold end coating in use today for NR glass containers. This coating is applied as a highly atomised spray of a dilute aqueous suspension of solid polyethylene particles. The coating is deposited as numerous dried, circular droplets on the glass surface, as shown in figure 2⁽⁶⁾. Normally, the dried droplets do not overlap and consequently, the polyethylene cold end coating does not completely cover the glass surface. However, when excessive amounts of polyethylene are deposited, complete surface coverage is observed and the glass is essentially encapsulated by the polymer coating.

When these hot end and cold end coatings are properly applied, they provide excellent surface lubricity and scratch protection under both dry and wet sliding conditions, with no associated performance problems

relative to the adhesion of paper labels when using common glues. However, if certain glues are used that are incompatible with the coatings on the glass surfaces, then some interference with proper label adhesion can be anticipated.

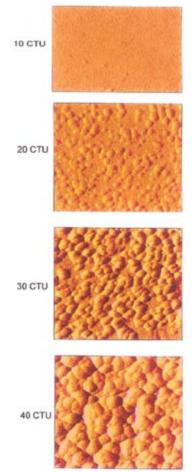
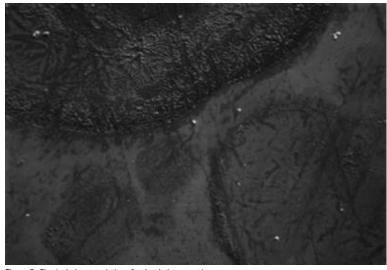


Figure 1: Physical characteristics of tin oxide coatings.







For example, dextrin type glues, initially intended for non-coated refillable bottles, are not tolerant of the chemistry and surface energy of glass surfaces that are well coated with both tin oxide and polyethylene. Therefore, this glue will not perform well when used to label well coated NR glass containers.

Conversely, synthetic glues have been developed for polymer surfaces and as a consequence, are very tolerant of even well coated glass surfaces and will result in complete label adhesion for NR glass containers. However, purely synthetic glues are relatively expensive and difficult to use in commercial practice and are not employed on a routine basis for NR glass containers. Therefore, fillers tend to utilise glues such as casein or blends of glues that allow easy use on well coated bottles at a reasonable cost.

In addition, it has been observed in previous, unreported tests that the deposition of excessive amounts of polyethylene results in complete coverage of the glass surface. This changes the chemical nature of the container surface from glass to essentially plastic. Other than synthetic glues, most other types of adhesives intended for use with glass containers will not function well when applied onto a 'plastic' surface.

EXPERIMENTAL PROCEDURE

Small capacity flint glass food jars were used as the substrates in the current study. These were commercially manufactured and coated with tin oxide from MBTC at three hot end thickness ranges. These ranges were: 0-10 CTU, 25-40 CTU and greater than 50 CTU (see 7 and $^{8)}$ for a definition of a CTU and how it is measured.

The lowest range was used in this study as a comparative baseline of essentially uncoated surfaces. The middle range was typical of hot end coating thicknesses that are applied onto NR glass containers in normal commercial practice. The highest thickness range was chosen as the values at which the hot end coating is essentially a thin continuous film, which exhibits consistent chemical and performance properties ^(1,4,5).

Polyethylene coatings were applied to the sample containers in the laboratory under carefully controlled conditions on rotating bottles to assure uniform vertical and circumferential distributions. The deposition parameters were adjusted to deposit coatings that replicated normal commercial amounts, as well as amounts that would be considered excessive and likely to interfere with proper label adhesion. A third set of samples was also created that were not coated with polyethylene. These were used as the second set of baseline samples in this study.

The polyethylene material that was used in these studies consisted of Duracote that was diluted to the normal commercial concentration of 100 parts of deionised water to one part of the Duracote concentrate. This coating was applied through an atomising spray gun onto the sample containers at a glass temperature of 120°C.

The extent to which the glass surface was covered by the polyethylene cold end coating was determined by a contact angle

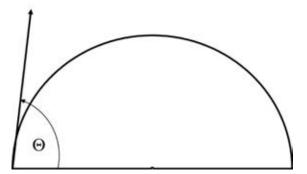


Figure 3: Profile of a liquid droplet for contact angle measurements.

technique. In this technique, a 10 micro-litre droplet of deionised water was placed onto the glass surface while the test bottle was held in a horizontal position on the stage of an optical comparator. The angle that the periphery of the droplet made with the glass surface was then measured, as shown in figure 3. These measurements were made on each of the test bottles at six evenly spaced circumferential locations and at two vertical heights corresponding to the location where the labels were to be subsequently applied.

It has been determined in prior experimentation at AGR that contact angle values are correlated to the degree to which the glass surface has been covered by the polyethylene coating (see figure 4). For example, a contact angle of 50 degrees is indicative of a glass surface that is one-half covered by polyethylene and a contact angle of 75 degrees is indicative of a glass surface that is completely covered by the polyethylene. Contact angle values greater than 75 degrees are indicative of additional layers of polyethylene coating in which the surface energy is reduced and the glass surface becomes increasingly hydrophobic.

For simplicity, only a casein glue was used in this study. This adhesive was typical of casein glues used for NR glass containers under normal filling line conditions. A typical commercial paper patch-style label was also used.

The casein glue was manually distributed in a uniform manner across the back of each test label by use of a #20, RDS draw-down rod. The labels were then immediately applied to the test containers and held under hand pressure for a few seconds to assure intimate contact with the glass surfaces. Two labels were applied to each of 10 test containers for each combination of tin oxide coating thickness range and polyethylene surface coverage group.>

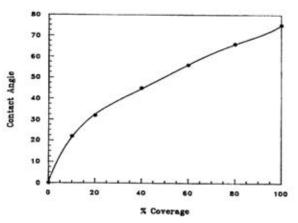


Figure 4: Relationship between contact angle and surface coatings for polyethylene cold end coatings.

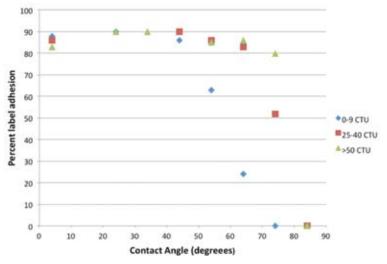


Figure 5: Label adhesion as a function of surface coverage and tin oxide coating thickness.

The labeled containers were stored for 24 hours under normal ambient laboratory conditions and the percent label adhesion was then determined manually by a standard 180 degree peel test. The percent label adhesion was recorded as the percentage of the original label area that remained affixed to the glass surface. After the label adhesion tests, the thickness of the hot end coating was measured by use of an AGR Hot End Coating Measurement System (HECMS). These measurements were made at three evenly spaced locations, just above and just below the area where the label had been applied.

Data collected for each test container included the percent label adhesion of each of the two test labels, the average tin oxide coating thickness around the perimeter of each of the two labels and the average contact angle in the area where each of the two labels were applied. The percent adhesion data were grouped by the three tin oxide hot end coating ranges (<10 CTU, 25-40 CTU and 50+ CTU) and for each decade of contact angle values (for example: 0-9 degrees, 10-19 degrees, 20-29 degrees etc, up to 80-89 degrees). For each decade, the average label adhesion was

calculated and plotted as a function of the median contact angle value for that specific decade.

DISCUSSION OF RESULTS

As shown by the data in figure 5, label adhesion was greater than 80% for both the normal commercial hot end thickness range and for the high hot end thickness range for contact angles up to approximately 74 degrees. At higher contact angles, the percent label adhesion decreased and finally reached 0% for contact angles of 84 degrees and greater. Data for the lower hot end coating thickness range (0-9 CTU) exhibited a different trend. The percent label adhesion began to decline at contact angles of about 54 degrees and eventually reached complete failure at a contact angle of about 74 dearees.

These data indicated that with a casein-type glue, label adhesion was very good and essentially identical for both normal hot end coating thicknesses and high levels of hot end coating thicknesses up to and slightly beyond complete surface coverage by the polyethylene coating. In addition, the current data show that for the normal range of commercially deposited polyethylene (contact angle range of 50 to 75



degrees), hot end coatings will neither improve nor detract from proper label adhesion. These results are in agreement with previous unreported data that have been obtained in the American Glass Research laboratory and show that casein-type adhesives are relatively tolerant of polyethylene coatings.

However, when the hot end coating was substandard, label adhesion decreased significantly in the normal range of polyethylene surface coverage (50 to 75 degrees) and was completely lost once complete surface coverage was reached. Thus, the absence of hot end coating causes label adhesion to diminish in the normal range of polyethylene coverage.

It should be noted that when diagnosing label adhesion problems, the first and most critical attribute is the level to which the polyethylene coating has covered the glass surface. This can be easily determined through the use of the contact angle technique. Hot end coating thicknesses can be considered and easily evaluated by the use of commercially available coating meters. Since hot end coating thicknesses are routinely monitored and carefully controlled in commercial practice to assure adequate surface lubricity and protection, it would be unusual to find that the lack of sufficient hot end coating would be the sole cause of label adhesion problems.

REFERENCES

- G L Smay, J S Wasylyk and R D Southwick, 'A critical assessment of lubricating and damage-preventive glass coatings', The Eitel Institute for Silicate Research, Third Proceeding of the Symposium, March, 22, 1982, pp 39.
- F Geotti-Bianchini and Martina Preo, 'Analysis of polyethylenebased cold end coatings on glass containers with contact angle and IR spectroscopy', Glastechn Ber Glass Science and Technology, 72, No 11, pp 341.
- Carlo Pantano, Vince J Bojan and Gary Smay, 'AFM analysis of hot end coatings on glass containers', The Glass Researcher, Vol 9, No 2, spring 2000, pp. 12
- 2, spring 2000, pp 12.
 Joerg Von Samson, 'Glass coating a key to quality improvements', AFGM Conference, Cebu, Phillippines, November 1989 (Glass Machinery Plants and Accessories), pp 35.
- Gary Smay, 'Surface energy determinations of tin oxide coated soda-lime-silica glass', J Am Ceram Soc, 71(4), 1988, pp C217.
- P W L Graham, 'Lubricious and protective coatings for glass containers', Proceedings 46th Conference on Glass Problems, Urbana III. Ceram Eng Sci Proc. 1986 7(34), pn 439
- Urbana, III, Ceram Eng Sci Proc, 1986, 7(3-4), pp 439.
 7. F Geotti-Bianchini, M Verita, L DeRiu and A Stella, 'Evaluation of tin oxide coatings on glass containers', Glass Technology, October, 1994, pp 216.
- N Jackson, J Ford, 'Experience in the control and evaluation of coatings on glass containers', Thin Solid Films, 77(1981), pp 23.

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